[Technical Data]
Proper Bolt Axial Tightening Force and Proper Tightening Torque
[Technical Data]
Strength of Bolts, Screw Plugs and Dowel Pins
1)Tensile Load Bolt
$=\sigma t \times A s \cdots \cdots(1)$
$=\pi d^{2} \sigma t / 4 \cdots(2)$


ExTThe proner siz of a hexagon sccket head can screws which is to beara r reneated tensile load pulustino

$0.7 \times 112 \times 20$.


| $\bar{a}$ | Tightening Method | Surface Condition |  | Lubrication |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Bolts | Nuts |  |
| 1.25 | Torque Wrench | Marganese Prosphate | Not treated or Treated with Pospphate. | Lubricated with oil or MoS2 paste |
| 1.4 | Torque Wrench | Not teated or Treatedwith Pospondit. |  |  |
|  | Limited-Torque Wrench |  |  |  |
| 1.6 | Impact Wrench |  |  |  |
| 1.8 | Torque Wrench |  | No Treatm | Unlubricat |
|  | Limited-Torque Wrench | with Phosphate. |  | Unlubricat |


Finol incrixion 0.185 SCM-AL FC-AL AL-SUS

$0.215 \mathrm{AL}-\mathrm{AL}$
Strength Class
seab But 0.35 STOC-SCM SCM-SCM FC-S10C FC-SCM AL


-The minimum value of tensile sterength is $1220 \mathrm{~N} / \mathrm{m}^{2}\left\{124 \mathrm{~kg} / \mathrm{mm}^{2}\right\}$


$\square$ Initial Tightening Force and Tightening Torque
Strength Class

| Nominal of Thread | $\begin{array}{\|c\|} \hline \text { Effective } \\ \text { Sectional Area } \\ \text { As } \\ \mathrm{mm}^{2} \end{array}$ | Strength Class |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 12.9 |  |  | 10.9 |  |  | 8.8 |  |  |
|  |  | Yield Load | linidiontering Foree | Tightering Torque | Yield Load | hidid Toptering Foree | Tightening Torque | Yield Load | Initid Toptering foree | Tightering Torue |
|  |  | kgf | kgf | kgf $\cdot \mathrm{cm}$ | kgf | kgf | kgf.cm | kgf | kgf | kgf $\cdot \mathrm{cm}$ |
| M 3 $\times 0.5$ | 5.03 | 563 | 394 | 17 | 482 | 338 | 15 | 328 | 230 | 10 |
| M 4×0.7 | 8.78 | 983 | 688 | 40 | 842 | 589 | 34 | 573 | 401 | 23 |
| M 5×0.8 | 14.2 | 1590 | 1113 | 81 | 1362 | 953 | 69 | 927 | 649 | 47 |
| M 6x1 | 20.1 | 2251 | 1576 | 138 | 1928 | 1349 | 118 | 1313 | 919 | 80 |
| M 8×1.25 | 36.6 | 4099 | 2869 | 334 | 3510 | 2457 | 286 | 2390 | 1673 | 195 |
| M10×1.5 | 58 | 6496 | 4547 | 663 | 5562 | 3894 | 567 | 3787 | 2651 | 386 |
| M12x1.75 | 84.3 | 9442 | 6609 | 1160 | 8084 | 5659 | 990 | 5505 | 3853 | 674 |
| M14×2 | 115 | 12880 | 9016 | 1840 | 11029 | 7720 | 1580 | 7510 | 5257 | 1070 |
| M16x2 | 157 | 17584 | 12039 | 2870 | 15056 | 10539 | 2460 | 10252 | 7176 | 1670 |
| M18×2.5 | 192 | 21504 | 15053 | 3950 | 18413 | 12889 | 3380 | 12922 | 9045 | 2370 |
| M20 2.5 | 245 | 27440 | 19208 | 5600 | 23496 | 16447 | 4790 | 16489 | 11542 | 3360 |
| M22×2.5 | 303 | 33936 | 23755 | 7620 | 29058 | 20340 | 6520 | 20392 | 14274 | 4580 |
| M24×3 | 353 | 39536 | 27675 | 9680 | 33853 | 23697 | 8290 | 23757 | 16630 | 5820 |

Note) - Tightening Conditions:Use of a torque wrench(Lubricated with Oil, Torque Coefficient $\mathrm{k}=0.17$, Tightening Coefficient $\mathrm{Q}=1.4$ )
The table is an excerpt trom a catalog of Kyokuto Seisakusho Co.,, tod.
(1)Using Equation

## As=Pt/ot <br> $89\left[m m^{2}\right.$

- finding a value greater than the result
of the equation in the Effective Sectiona
rea column in the table on right,
$5,14.2[\mathrm{~mm}$ ] , should be selected.
6, allowable load of 213 kgf , should be selected from the column for
strength class 12.9 , with the fatigue strength taken into account.

2) If the bolt, like a stripper bolt, is to bear a tensile impact load, the right size should be selected from the fatigue strength column.(Under a load of 200 kgf , stripper bolt made of SCM435, 33 to 38 HRC, strength class 10.9
By finding a value greater than the allowable load of 200 kgf in the Strength Class 10.9 column in the table on right, M8, 318 kkgff , should be selected. Hence, MSB10 with the M 8 threaded portion and an axial diameter of 10 mm should be selected.
If it is to bear a shearing load, a dowel pin should also be used.

## Strength of Screw Plug

When screw plug MSW30 is to bear an impact load, allowable load P should be determined The materials of MSW30 are 545 C , 34 to 43 HRC , tensile strength ot $65 \mathrm{~kg} / / \mathrm{mm}^{2}$.)

| meter | Area $\mathrm{A}=$ Root Diameter $\mathrm{d} 1 \times \pi \times \mathrm{L}$ |
| :---: | :---: |
| becaluluted | (Root Diameter di $\sim M-$ P) |
|  | $\mathrm{A}=(\mathrm{M}-\mathrm{P}) \pi \mathrm{L}=(30-1.5) \pi \times 12$ $=1074\left[\mathrm{~mm}^{2}\right]$ |
| $\mathrm{d}=\tau \mathrm{t} \times \mathrm{A}$ |  |
| $=3.9 \times 107.4$ | Shearing Stress $\sim 0.8 \times$ Yield Stress |
| =4190[kgf] | $=46.6$ |
| able shearing force | Allowable Shearing Stress $\tau t=$ Shearing Stress/Safety Factor12 $=46.6 / 12=3.9\left[\mathrm{kgf}^{2} / \mathrm{mm}^{2}\right]$ |

Fin tre alowable stearing force thread if a tap is made of soft material.


## Strength of Dowel Pins

The proper size of a dowel pin under repeated shearing load of 800 kgf(Pulsating)
should be determined.(The material of Dowel Pins is SUJ2. Hardness 58HRC~)
$=\sqrt{(4 \times 800) /(3.14 \times 19.2)}$

$$
\begin{aligned}
& \text { Yield Stress for SUJ2 } \mathrm{ab}=120\left[\mathrm{kgf} / \mathrm{mm}^{2}\right] \\
& \text { Allowable Shearing Strength } \tau=\sigma b \times 0.8 / \text { Safety Factor } \alpha \\
& =19.2\left[\mathrm{kgg} / \mathrm{mm}^{2}\right]
\end{aligned}
$$

$\approx 7.3$
or a larger size should be selected for MS.

The yield stress, strength class 12.9, is $\sigma b=112\left[\mathrm{~kg} / \mathrm{mm} \mathrm{m}^{2}\right]$. Allowable Stess $\sigma t=\sigma$ b/Saxiety Factorf(rion the above tade Satey Factor 5) $=112 / 5$

| Nominal of Thread | Effectie <br> SectionA Aea <br> As <br> $\mathbf{m m}^{2}$ | Strength Class |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 12.9 |  | 10.9 |  |
|  |  | $\begin{array}{\|c\|c\|} \hline \text { Faitigue Stengut Allowable Lood } \\ \hline \mathrm{kgf} / \mathbf{m m}^{2} & \mathbf{k g f} \\ \hline \end{array}$ |  | Fative Stengith $\mathrm{kgg} / \mathrm{mm}^{2}$ | Alowade |
|  |  |  |  | kgf |
| M 4 | 8.78 | 13.1 | 114 |  | 9.1 | 79 |
| M 5 | 14.2 | 11.3 | 160 | 7.8 | 111 |
| M 6 | 20.1 | 10.6 | 213 | 7.4 | 149 |
| M 8 | 36.6 | 8.9 | 326 | 8.7 | 318 |
| M10 | 58 | 7.4 | 429 | 7.3 | 423 |
| M12 | 84.3 | 6.7 | 565 | 6.5 | 548 |
| M14 | 115 | 6.1 | 702 | 6 | 690 |
| M16 | 157 | 5.8 | 911 | 5.7 | 895 |
| M20 | 245 | 5.2 | 1274 | 5.1 | 1250 |
| M24 | 353 | 4.7 | 1659 | 4.7 | 1659 |



The dowel pin must not be loaded.
 extra pins can be reduced.
uniform size, the number of the necessary tools and
Typical strength calculations are presented here. In practice, further conditions including hole-to-hole pitch precision, hole perpendicularity, surface roughness, circuarity, plate material, parallelism, quenching or non-quenching, precision of the press, product output, wear of tools should be considered. Hence the values in these examples are typical but not guaranteed values.(Not guaranteed values)

